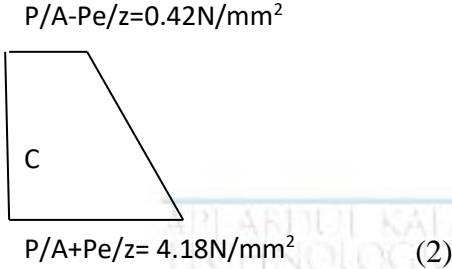
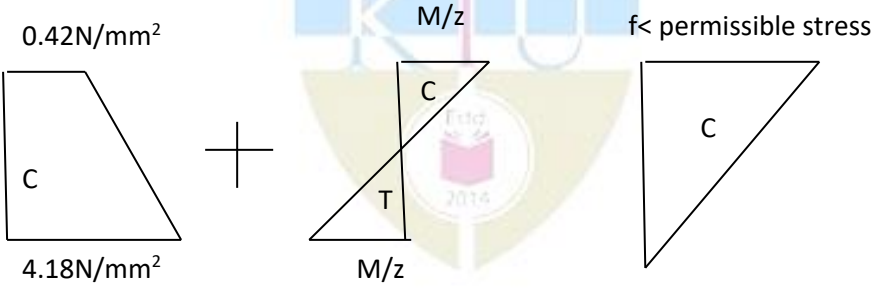


<b>Scheme of Valuation/Answer Key</b>			
(Scheme of evaluation (marks in brackets) and answers of problems/key)			
<b>APJ ABDUL KALAM TECHNOLOGICAL UNIVERSITY</b>			
SIXTH SEMESTER B.TECH DEGREE EXAMINATION, MAY 2019			
<b>Course Code: CE304</b>			
<b>Course Name: DESIGN OF CONCRETE STRUCTURES - II</b>			
Max. Marks: 100		Duration: 3 Hours	
<b>PART A</b>			
<i>Answer any two full questions, each carries 15 marks.</i>			Marks
1	a)	<p>Factored load and finding values of <math>P_u/f_{ck} bD</math> and <math>M_u/f_{ck} b D^2</math></p> $\frac{P_u}{f_{ck} bD} = \frac{1050 \times 10^3}{20 \times 300 \times 600} = 0.291$ $\frac{M_u}{f_{ck} D^2} = \frac{225 \times 10^6}{20 \times 300 \times 600^2} = 0.104 \quad (3)$ $\frac{d'}{D} = \frac{50}{600} = 0.083 = 0.1$ <p><math>f_y=250\text{MPa}</math>; Reinforcement equally on 2 sides; Chart 28 or reinforcement equally on 4 sides Chart 40, Finding <math>p/f_{ck}</math>, and <math>A_s</math> (2)</p> <p>Diameter and no. of bars (1)</p> <p>Design of lateral ties and spacing (2)</p> <p>Detailed cross section (2)</p>	(10)
	b)	<p>Calculation of additional moments-</p> $M_{ax} = \frac{P_u D}{2000} \left\{ \frac{l_{ex}}{D} \right\}^2$ $M_{ay} = \frac{P_u b}{2000} \left\{ \frac{l_{ey}}{b} \right\}^2$ <p style="text-align: center;">- (reduction factor – optional) — (2)</p> <p>Modified Initial moments = <math>0.4M_{a1} + 0.6M_{a2}</math></p> <p>Calculate moment due to minimum eccentricity and comparing with modified actual moments- greater value to be taken as initial moments for adding with the additional moments (2)</p> <p>Checking the section for axial load and biaxial bending (1)</p>	(5)

2	a)	<p>Check for slenderness ratio - 1</p> <p>Check for min eccentricity - 1</p> <p>Trial reinforcement and uniaxial moment capacities about x- and y- axes - 4</p> <p>Finding <math>P_{uz}</math> and <math>\alpha_n</math> - 3</p> <p>Checking interaction equation - 3</p> <p>Design of lateral ties and spacing - 2</p> <p>Detailing - 1</p> <p style="text-align: center;"><u>Alternate Solution</u></p> <p>Check for slenderness ratio - 1</p> <p>Check for min eccentricity - 1</p> <p>Trial reinforcement and uniaxial moment capacities about x- and y- axes - 4</p> <p><math>P_{uz}</math> from Chart 63 (3)</p> <p>For given <math>P_u/P_{uz}</math> and <math>M_{uy}/M_{uy1}</math>, calculate Permissible <math>M_{ux} / M_{ux1}</math> from Chart 64 (3)</p> <p>Design of lateral ties and spacing - 2</p> <p>Detailing - 1</p>	(15)
3	a)	<p>Total Load on footing including self weight = 2200kN (1)</p> <p>Calculation of base area and upward pressure (3)</p> <p>Thickness of footing based on one way shear (3)</p> <p>Check for two way shear (2)</p> <p>Design of flexural reinforcement (both directions) (3)</p> <p>Check for Development length (1)</p> <p>Detailing (2)</p>	15
<b>PART B</b>			
<i>Answer any two full questions, each carries 15 marks.</i>			
4	a)	<p>Assuming value of <math>\phi = 30^\circ</math></p> <p>Depth of foundation <math>D_f = \frac{p}{\gamma} \left( \frac{1 - \sin \phi}{1 + \sin \phi} \right)^2 = 1.2m</math> (1)</p> <p>Proportioning the retaining wall with figure (3)</p> <p>F.O.S against overturning = <math>\frac{0.9M_R}{M_o} &gt; 1.4</math> (2)</p>	(15)

		<p>F.O.S against sliding = <math>\frac{0.9\mu\sum W}{P_a} &gt; 1.4</math> (2)</p> <p>Upward soil pressure diagram and check (1)</p> <p>Design and detail the heel slab - 3</p> <p>Design and detail the toe slab - 3</p>	
5	a)	<p>Circumstances - 2</p> <p>design procedure - 4</p> <p>Detailing- 4</p>	(10)
	b)	<p>Calculation of radius of sphere from span and rise (1)</p> <p>Meridional stress = <math>\frac{wR(1 - \cos\theta)}{t \sin^2 \theta} = \frac{wR}{t(1 + \cos\theta)}</math></p> <p>Hoop stress = <math>\frac{wR(\cos^2 \theta + \cos\theta - 1)}{t(1 + \cos\theta)}</math></p> <p>If stresses are minimal, nominal reinforcement to be provided (3)</p> <p>Design of ring beam based on stress on equivalent area (1)</p>	5
6	a)	<p>Load calculation (w kN/m<sup>2</sup>) (2)</p> <p>For fixed edges,</p> <p>At Centre, <math>M_r = \frac{wr^2}{16}</math>      <math>M_\theta = \frac{wr^2}{16}</math></p> <p>At edges, <math>M_r = -\frac{wr^2}{8}</math>      <math>M_\theta = 0</math> (2)</p> <p>Check for depth (1)</p> <p>Reinforcement at centre (3)</p> <p>Reinforcement at edge- (3)</p> <p>Check for shear (1)</p> <p>Detailing (3)</p>	15
<b>PART C</b>			
<i>Answer any two full questions, each carries 20 marks.</i>			
7	a)	<p>Volume = 500m<sup>3</sup></p> <p>Height and diameter of tank (3)</p>	(20)

		<p>As per IS 3370 (2), minimum strength of concrete for water tanks is M25. So, this can be mentioned and stresses for M25 can be adopted for the design.</p> <p>Either fixed or hinged base can be assumed.</p> <p>Assuming suitable thickness of wall, calculate <math>H^2/Dt</math></p> <p>Hoop tension = coefficient(wHR) (2)</p> <p>Moment= coefficient(wH<sup>3</sup>) (2)</p> <p>Shear= coefficient (wH<sup>2</sup>) (2)</p> <p>Design of horizontal rings based on Hoop tension (3)</p> <p>Design of vertical reinforcement based on moment (3)</p> <p>Check for shear stress (1)</p> <p>Design of base slab (As it is resting on ground, nominal thickness and minimum reinforcement can be provided (2)</p> <p>Detailing with haunches (2)</p>	
8	a)	<p><b>Listing – 3</b></p> <p>Immediate Losses include</p> <ol style="list-style-type: none"> <li>i. Elastic Shortening of Concrete</li> <li>ii. Slip at anchorages</li> <li>iii. <u>Friction</u> between tendon and tendon duct, and <u>wobble Effect</u></li> </ol> <p>2. Time Dependent Losses include</p> <ol style="list-style-type: none"> <li>i. Creep and Shrinkage of concrete</li> <li>ii. Relaxation of prestressing steel</li> </ol> <p><b>Explanation – 2</b></p>	(5)
	b)	<p>Loss due to friction = <math>f_0(\mu\alpha + kx) = 102.7\text{N/mm}^2</math> (5)</p> <p>Loss due to slip = <math>\frac{\delta}{L} E_s = 70\text{ N/mm}^2</math> (5)</p> <p>Total loss – 172.7 N/mm<sup>2</sup></p> <p>Percentage loss – 17.2% (2)</p> <p>Final force = f A = 496.38 kN (3)</p>	15
9	a)	<b>Explanation - 4</b>	4

	<p>b) Why high strength concrete – 3 Why high strength steel - 3</p>	6
	<p>c) <math>P=700(\pi/4 \times 12 \times 12)4=316.5\text{kN}</math> (1)</p> <p><math>e=275-200=75\text{mm}</math></p> <p><math>P/A= 2.3\text{N/mm}^2</math>      <math>Pe/z=1.88\text{N/mm}^2</math> (2)</p> <p>Assuming moment due to self weight to be negligible, stress diagram at transfer of prestress is</p> <div style="text-align: center;">  <p><math>P/A-Pe/z=0.42\text{N/mm}^2</math></p> <p><math>P/A+Pe/z= 4.18\text{N/mm}^2</math> (2)</p> </div> <p>Let M be the total BM including that due to self weight</p> <p>For no tension to be developed in the section, net stress at bottom = 0</p> <div style="text-align: center;">  <p><math>0.42\text{N/mm}^2</math>      <math>M/z</math>      <math>f &lt; \text{permissible stress}</math></p> <p><math>4.18\text{N/mm}^2</math>      <math>M/z</math></p> </div> <p><math>4.18-M/z = 0</math></p> <p><math>M= 52.63 \text{ kNm}</math> (inclusive of moment due to self weight). (3)</p> <p>Since the span of the beam is not mentioned, BM due to dead load can't be calculated.</p> <p>Check: stress at top = <math>0.42+ 4.18 = 4.6 \text{ N/mm}^2 &lt; \text{permissible compressive stress for concrete.}</math> (2)</p>	10
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