

| 3 | a) | $\begin{aligned} & \varphi \text { index is } 22 \mathrm{~mm} / \mathrm{hr} \\ & \text { duration of measurement }=30 \mathrm{~min}=0.5 \mathrm{hr} \\ & \text { when rate of precipitation is less than } \varphi \text { index, no runoff occur }-1 \text { mark } \\ & \text { Runoff depth }=[(24-22)+(36-22)+(28-22)] \times 0.5=\underline{\mathbf{1 1 m m}}-2 \text { marks } \\ & \text { Area of catchment }=30 \mathrm{~km}^{2} \\ & \text { runoff volume from the catchment }=\left(30 \times 10^{6}\right) \times(11 / 1000)=\frac{\mathbf{3 3 \times 1 \mathbf { 1 0 } ^ { 4 } \mathbf { m } ^ { 3 }}}{-2 \text { marks }} \end{aligned}$ |  |  |  |  |  |  | (5) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | b) | S curve derivation-4marks  <br> Lag by 9hr, difference hydrograph -3 marks <br> 9hr UHO = diff. hydrograph ordinates x (6/9) -3 marks |  |  |  |  |  |  | (10) |
|  |  | Time <br> (hrs) | $\begin{gathered} \hline 6 \mathrm{hr} \\ \mathrm{UHO} \\ \mathrm{~m} 3 / \mathrm{s} \\ \hline \end{gathered}$ | S curve addition | S curve | lagged <br> by 9 hr | difference <br> hydrograph | 9hr UHO $\mathrm{m} 3 / \mathrm{s}$ |  |
|  |  | 0 | 0 |  | 0 |  | 0 | 0.00 |  |
|  |  | 3 | 9 |  | 9 |  | 9 | 6.00 |  |
|  |  | 6 | 20 | 0 | 20 |  | 20 | 13.33 |  |
|  |  | 9 | 35 | 9 | 44 | 0 | 44 | 29.33 |  |
|  |  | 12 | 49 | 20 | 69 | 9 | 60 | 40.00 |  |
|  |  | 15 | 43 | 44 | 87 | 20 | 67 | 44.67 |  |
|  |  | 18 | 35 | 69 | 104 | 44 | 60 | 40.00 |  |
|  |  | 21 | 28 | 87 | 115 | 69 | 46 | 30.67 |  |
|  |  | 24 | 22 | 104 | 126 | 87 | 39 | 26.00 |  |
|  |  | 27 | 17 | 115 | 132 | 104 | 28 | 18.67 |  |
|  |  | 30 | 12 | 126 | 138 | 115 | 23 | 15.33 |  |
|  |  | 33 | 9 | 132 | 141 | 126 | 15 | 10.00 |  |
|  |  | 36 | 6 | 138 | 144 | 132 | 12 | 8.00 |  |
|  |  | 39 | 3 | 141 | 144 | 138 | 6 | 4.00 |  |
|  |  | 42 | 0 | 144 | 144 | 141 | 3 | 2.00 |  |
|  |  | 45 | 0 | 144 | 144 | 144 | 0 | 0.00 |  |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  | PAR |  |  |  |  |
|  |  |  | Answer | y two fult | uestions, | each carr | es 15 marks. |  |  |
| 4 | a) | Difference betwee | erennial | nd inunda | on irrigati |  |  |  | (3) |
|  | b) | Definition of duty relationship betwe $\Delta$-delta in m;, BDerivation of relat | Delta <br> hem - $\Delta$ <br> period <br> ship | $\begin{aligned} & =8.64 \mathrm{~B} / \mathrm{D} \\ & \mathrm{n} \text { days } ; \mathrm{D} \end{aligned}$ | - duty in h | cumec | $\begin{gathered} -2 \mathrm{n} \\ -2 \mathrm{n} \\ -2 \mathrm{~m} \end{gathered}$ |  | (6) |
|  | c) | gross command ar Duty $=8.64 \mathrm{~B} / \Delta-$ intensity of irrigat area of irrigation $=$ kor period = 15 da | 2000 h <br> ark <br> for whea <br> $00 \times 50 /$ <br> or depth | $\begin{aligned} & =50 \% \\ & 00=1000 \mathrm{~h} \\ & =15 \mathrm{~cm} \end{aligned}$ |  |  |  |  | (6) |


|  |  | ```Duty \(=8.64 \times 15 / 0.15=864\) ha/cumec discharge required \(=\) area/duty \(=1000 / 864=\mathbf{1 . 1 5}\) cumec \(\quad-2\) marks intensity of irrigation for gram \(=30 \%\). area of irrigation \(=2000 \times 30 / 100=600 \mathrm{ha}\) kor period \(=18\) days kor depth \(=12 \mathrm{~cm}\) Duty \(=8.64 \times 18 / 0.12=1296\) ha/cumec discharge required \(=\) area/duty \(=600 / 1296=0.46\) cumec \(\quad-2\) marks total discharge required \(=\underline{\mathbf{1 . 1 5}}\) cumec- 1 mark (Both are Rabi crops)``` |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5 | a) | Explanation of different flooding methods of irrigation |  |  |  |  |  |  |  |  |  | (5) |
|  | b) | Definition of (i) root zone depth (ii) permanent wilting (ii) consumptive use (iv) conveyance efficiency $4 \times 1=4$ marks |  |  |  |  |  |  |  |  |  | (4) |
|  | c) | ```Area of crop \(=3000\) ha; Field capacity of soil \(=26 \%\); Optimum moisture \(=12 \%\) permanent wilting point \(=10 \%\); Eff. depth of root zone \(=80 \mathrm{~cm}\); relative density of soil \(=1.4\); frequency of irrigation \(=10\) days; \(\quad\) overall efficiency \(=23 \%\). \(\mathrm{d}_{\mathrm{w}}=\gamma_{\mathrm{d} . \mathrm{d}} \mathrm{d}(\mathrm{FC}-\mathrm{OMC}) / \gamma_{\mathrm{w}}=1.4 \mathrm{x} 0.8(0.26-0.12)=15.68 \mathrm{~cm}\) \(\mathrm{C}_{\mathrm{u}}=15.68 / 10=\underline{\mathbf{1 . 5 6 8} \mathbf{~ c m}} \quad-3\) marks Discharge \(=3000 \times 10^{4} \times(1.568 / 100) /(24 \times 3600)=\mathbf{5 . 4 5 m} \mathbf{m}^{3} / \mathrm{sec} \quad-2\) marks Discharge of canal \(=5.45 \times 100 / 23=23.695 \mathrm{~m}^{3} / \mathrm{sec} \quad-1\) mark``` |  |  |  |  |  |  |  |  |  | (6) |
| 6 | a) | stage discharge curve - sketch -2 marks <br> - discussion -2 marks |  |  |  |  |  |  |  |  |  | (4) |
|  | b) | objectives of river training (at least 4) - listing only-2 marks repelling, attracting and deflecting groynes (with sketch) |  |  |  |  |  |  |  |  |  | (5) |
|  | c) | area is computed by multiplying depth of flow at vertical by width of strip which is taken halfway to adjacent verticals on either side |  |  |  |  |  |  |  |  |  | (6) |
|  |  | Distance from bank | $\begin{gathered} \text { Flow } \\ \text { depth } \mathbf{d}) \\ \mathbf{m} \end{gathered}$ | Meter depth $m$ | $\begin{gathered} \text { no. } \\ \text { of } \\ \text { rev } \end{gathered}$ | time sec | N rev/s | v m/s | $\begin{aligned} & \mathbf{V}_{\mathrm{av}} \\ & \mathrm{~m} / \mathrm{s} \end{aligned}$ | $\begin{gathered} \text { area } \\ \mathbf{m}^{2} \end{gathered}$ | q m $3 / \mathrm{s}$ |  |
|  |  | 0 | 0 |  |  | - | - |  | - | - | - |  |
|  |  | 0.8 | 0.5 | 0.3 | 12 | 48 | 0.25 | 0.125 | 0.125 | 0.4 | 0.050 |  |
|  |  | 1.6 | 1 | 0.8 | 23 | 52 | 0.44 | 0.183 | 0.222 | 0.8 | 0.178 |  |
|  |  | - | - | 0.2 | 36 | 51 | 0.71 | 0.262 |  |  |  |  |
|  |  | 2.4 | 1.6 | 1.28 | 27 | 54 | 0.50 | 0.200 | 0.228 | 1.12 | 0.255 |  |
|  |  | - | - | 0.32 | 41 | 60 | 0.68 | 0.255 |  |  |  |  |
|  |  | 3 | 1.8 | 1.44 | 28 | 53 | 0.53 | 0.208 | 0.238 | 1.26 | 0.300 |  |
|  |  | - | - | 0.36 | 42 | 58 | 0.72 | 0.267 |  |  |  |  |
|  |  | 3.8 | 1.2 | 0.96 | 24 | 50 | 0.48 | 0.194 | 0.227 | 0.96 | 0.218 |  |
|  |  | - | - | 0.24 | 35 | 50 | 0.70 | 0.260 |  |  |  |  |
|  |  | 4.6 | 0.6 | 0.36 | 14 | 45 | 0.31 | 0.143 | 0.143 | 0.48 | 0.069 |  |
|  |  | 5.2 | 0 | - | - | - | - | - | - | - | - |  |
|  |  | $1.069$ <br> *(Velocity using current meter is measured at 0.6 d near two banks. At other verticals ,it is |  |  |  |  |  |  |  |  |  |  |


|  |  | measured at $0.8 d$ and 0.2 d . So the average velocity has to be calculated using the corresponding velocities at 0.8 d and $0.2 d$. At the banks, Average velocity at the Banks is the velocity corresponding to $0.6 d$. Area is computed by multiplying depth of flow at vertical by width of strip which is taken halfway to adjacent verticals on either side) <br> *As the given question is an above average question, full credit is to be given, if correct steps are followed by the candidate |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PART C |  |  |  |  |  |  |  |  |
| Answer any two full questions, each carries 20 marks. |  |  |  |  |  |  |  |  |
| 7 | a) | Flow duration curve - fig <br> - Explanation <br> - Applications |  |  |  | $\begin{aligned} & -2 \text { marks } \\ & -2 \text { marks } \\ & -2 \text { marks } \end{aligned}$ |  | (6) |
|  | b) | Explanation of process of reservoir sedimentation Control measures of reservoir sedimentation |  |  |  | $\begin{aligned} & \hline-3 \text { marks } \\ & -3 \text { marks } \\ & \hline \end{aligned}$ |  | (6) |
|  | c) | determining reservoir capacity fig of mass curve showing salient points-3 marks step by step procedure -5 marks |  |  |  |  |  | (8) |
| 8 | a) | various factors affecting selection of site for a reservoir (at least 6 factors) |  |  |  |  |  | (6) |
|  | b) | initial <br> annual <br> vol. of <br> sedime$\%$ <br> 100 <br> 80 <br> 60 <br> 40 <br> 20 | capacity $=50 \mathrm{mi}$ sediment inflow sediment inflow nt trapped $\mathrm{St}=$ | on cu.m, average inf 300,000 tons, dens $=300,000 \times 1000 / 12$ <br> $x \eta-3$ marks | w rate $=$ of sedim $50=0.24 x$ $\qquad$ <br> av. $\eta$ <br> 0.9735 <br> 0.965 <br> 0.955 <br> 0.935 <br> 174.1yea | illion cu.m <br> $=1250 \mathrm{~kg} / \mathrm{m}$ <br> $\mathrm{m}^{3} / \mathrm{year}$St <br> $\left(\mathrm{x} 10_{6} \mathrm{~m} 3\right)$0.2340.23160.2292 | years tofill(10/st) $4^{42.7}$43.2 <br> 43.6 <br> 44.6 <br> -6 marks | (9) |
|  | c) | Definition of Porosity, specific yield ,specific retention.-3 marks relation between them [ porosity $=\mathrm{s}_{\mathrm{y}}+\mathrm{S}_{\mathrm{r}}$ ] <br> -2 marks |  |  |  |  |  | (5) |
| 9 | a) | Darcy's law - statemen <br> -Formula <br> -Derivati |  |  |  | -1 marks-1 marks-3 marks |  | (5) |
|  | b) | expression for steady radial flow in a confined aquifer - fig-2 marks <br> - Expression $\left[\mathrm{Q}=2 \Pi \mathrm{~T}\left(\mathrm{~s}_{2}-\mathrm{s}_{1}\right) / \log _{\mathrm{e}}\left(\mathrm{r}_{1} / \mathrm{r}_{2}\right)\right]$ <br> -2 marks <br> - Derivation steps-4 marks |  |  |  |  |  | (8) |
|  | c) | $\begin{aligned} & \mathrm{Q}=\text { CAH }-1 \text { mark } \\ & \mathrm{h}_{1}=250-243=7 \mathrm{~m} ; \mathrm{h}_{2}=250-245=5 \mathrm{~m} \end{aligned}$ |  |  |  |  |  | (7) |


|  | $\mathrm{t}=2 \mathrm{hr} ; \mathrm{H}=3 \mathrm{~m} ; \mathrm{A}=\Pi\left(5^{2}\right) / 4=19.64 \mathrm{~m}^{2}$ <br> ( As the diameter of the well is not specified in the question, full credits may be given to those calculated with any assumed diameter) - 2 marks $\begin{array}{lr} \mathrm{C}=2.303\left(\log _{10}\left(\mathrm{~h}_{1} / \mathrm{h}_{2}\right) / \mathrm{t}\right. & -1 \mathrm{mark} \\ =0.1683 / \mathrm{hr} & -2 \mathrm{marks} \\ \mathrm{Q}=\underline{\mathbf{9 . 9 1 8 m}}{ }^{3} / \mathbf{s}=\mathbf{2 . 7 5 5 l i t r e s} / \mathbf{s e c}-1 \mathrm{mark} & \end{array}$ |  |  |
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| **** |  |  |  |

